

Combined use of k-effective and beta-effective measurements for nuclear data validation and improvement

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PURPOSE

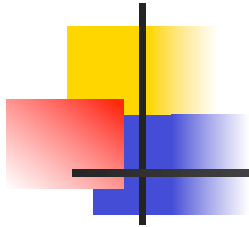
- Mainly criticality benchmarks are used for ND validation and adjustment studies. However, k_{eff} is a very global parameter;
- Validation against other type of measurements provides a complementary view and wider scope validation;
- The following experimental measurements can be useful for ND validation & adjustment:
 - Critical benchmarks
 - **Kinetics measurements**
 - Shielding benchmarks



Motivation:

- Uncertainty in the effective delayed neutron fraction β_{eff} was studied in the in the scope of **UAM project of OECD/NEA since ~2010.**
- β_{eff} is important for:
 - dynamic behaviour of a reactor and safety analysis (\$): present and future reactor design (GEN-IV, ADS)
- **CHANDA project:** k_{eff} and β_{eff} sensitivity & uncertainty analyses of the **MYRRHA reactor.**
- **WPEC-SG39**

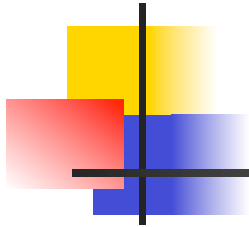
Effective delayed neutron fraction β -eff



$$\beta_{eff} = \frac{\nu_d}{k_{eff}} \frac{\partial k_{eff}}{\partial \nu_d}$$
$$= \int \Phi^+(\vec{r}, E', \Omega') \chi_d(E') dE' d\Omega' \int \nu_d(E) \Sigma_f(\vec{r}, E) \Phi(\vec{r}, E, \Omega) dE d\Omega d\vec{r}$$

- β_{eff} can be easily calculated using deterministic and Monte Carlo GPT codes;
- Sensitivity of β_{eff} can be obtained as a 2nd derivative of k_{eff} (Monte Carlo codes).

Bretscher's Prompt k Ratio Method for determining b-eff



$$\beta_{eff} = 1 - \frac{k_p}{k}$$

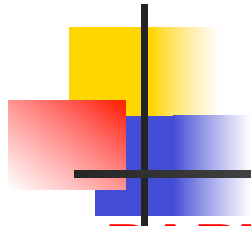
k : usual multiplication factor

k_p : multiplication factor with delayed neutrons not taken into account

Sensitivity of b-eff can be obtained as a (properly weighted) difference between two standard sensitivity terms:

$$\frac{\sigma}{\beta_{eff}} \frac{\partial \beta_{eff}}{\partial \sigma} = \frac{1 - \beta_{eff}}{\beta_{eff}} (S_k - S_{kp})$$

Sensitivity/uncertainty analysis - XSUN-2016 computational tool



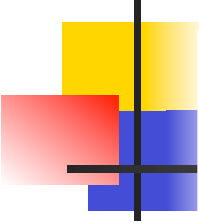
- **PARTISN**: 1D, 2D, 3D S_N transport solver (deterministic);
- **Cross sections**:
 - **ENDF/B-VII.1 33-group** cross-sections for **110 isotopes**, $T = 300$ to 850 K: processed by **NJOY-99** in MATXS format, self-shielded case dependent XS prepared by **TRANSX**;
- **SUSD3D** sensitivity-uncertainty calculations,
- **Covariance matrices**:
 - **JENDL-4.0** (delayed nu-bar), COMMARA-2, SCALE-6.0, ENDF/B-VII.1
- Validation against M/C:
 - Winfried Zwermann: XSUSA
 - Manuele Aufiero: SERPENT2 GPT extended



SUSD3D β_{eff} S/U analysed benchmarks from ICSBEP and IRPhE

- **SNEAK-7A & -7B:** MOX fuel reflected by metallic depleted U.
- **Jezebel:** bare sphere of ^{239}Pu metal, 6.385-cm radius
- **Skidoo** (Jezebel-23): bare $\sim 98.1\%$ ^{233}U sphere;
- **Popsy** (Flatop-Pu): ~ 20 -cm natural U reflected ^{239}Pu sphere;
- **Topsy** (Flatop-25): ~ 20 -cm natural U reflected ^{235}U sphere;
- **Flatop-23:** ~ 20 -cm natural U reflected ^{233}U sphere;
- **Big Ten:** 10% enriched U with U-reflector, cylinder $r=41.91\text{cm}$, $h=96.428\text{cm}$;
- **ZPPR-9:** MOX core with sodium cooling, depleted U blanket.
- **MYRRHA:** ADS

Calulated & measured b-eff



Benchmark	Measured (pcm)	Calculated (pcm)		
		SUSD3D	Prompt k-ratio	
			PARTISN	MCNP
SNEAK 7A	395±5.15%	373	379	369
SNEAK 7B	413±6%	419	429	415
Jezebel	195±5%	185	186	186
Jezebel- ²³³ U	290±3.5%	296	297	
Flattop-Pu	276±2.5%	277	278	284
Flattop- ²³⁵ U	665±2%	688	690	
23 Flattop	360±2.5%	374	375	
Big-ten	720±1%	720	734	
ZPPR-9P	/	360	362	
MYRRHA	/	322	323	

FLATTOP-23: Total uncertainty in b-eff: 5.5/6.9 %

($b_{\text{exp}} = 395$ pcm)

b (pcm):

^{233}U : 260

^{235}U : 650


$^{238}\text{U}_f$: 1480

MAT	Sensitivity (%/%)						
	elastic	inelastic	(n, f)	(n, γ)	$\bar{\nu}_d$	$\bar{\nu}_p$	$\bar{\nu}_t$
^{233}U	-0.005	-0.034	-0.230	-0.016	0.697	-0.882	-0.184
^{234}U	$2 \cdot 10^{-5}$	-0.001	-0.001	$-2 \cdot 10^{-4}$	0.007	-0.009	-0.002
^{235}U	0.001	-0.001	0.015	-0.001	0.015	0.002	0.017
^{238}U	0.074	-0.129	0.166	-0.033	0.273	-0.104	0.170

MAT	Uncertainty (%)								
	elastic	inelastic	(n, f)	(n, γ)	$\bar{\nu}_d$	$\bar{\nu}_p$	χ_p	χ_d	Total
JENDL-4.0m									
^{233}U	0.089	0.584	0.209	0.217	5.097	0.657	0.304	0.762	5.27
^{235}U	0.004	0.009	0.063	0.001	0.048	0.002	0.017	0.001	0.06
^{238}U	0.318	1.293	0.103	0.073	0.916	0.061	0.045	0.110	1.63
Sum	0.33	1.42	0.24	0.23	5.18	0.81	0.31	0.77	5.5
COMARA-2									
^{233}U	0.298	0.432	0.195	0.227	6.444	0.197	0.227	N/A	6.47
^{235}U	0.003	0.004	0.006	0.010	N/A	0.001	0.013	N/A	0.01
^{238}U	1.770	2.430	0.088	0.046	N/A	0.122	0.036	N/A	2.44
Sum	1.77	2.47	0.21	0.23	6.44	0.23	0.23	N/A	6.9



SNEAK-7B: Uncertainty in b_{eff} (TOTAL~3 %)



SNEAK-7B		Sensitivity (%/%)					
MAT	elastic	inelastic	(n,f)	(n, γ)	v_{del}	v_{pint}	v
U-235	$-2 \cdot 10^{-4}$	-0.002	0.060	-0.001	0.111	-0.052	0.059
U-238	-0.018	-0.160	0.261	0.011	0.550	-0.326	0.224
Pu-239	-0.001	-0.008	-0.228	-0.001	0.292	-0.565	-0.273

SNEAK-7B		Uncertainty (%)							
MAT.	elastic	inelast.	(n,f)	(n, γ)	v_{del}	v_{pint}	χ_p	χ_d	TOTAL
JENDL 4.0m									
U-235	~0	0.023	0.079	0.005	0.329	0.011	0.071	0.086	0.35
U-238	0.051	1.701	0.112	0.067	1.848	0.196	0.046	0.469	2.57
Pu-239	0.003	0.086	0.055	0.012	1.162	0.099	0.489	0.195	1.29
SUM	0.17	1.72	0.18	0.07	2.21	0.22	0.50	0.52	2.9
COMMARA-2									
U-235	0.009	0.010	0.028	0.011	N/A	0.005	0.051	/	0.06
U-238	2.863	2.991	0.139	0.046	N/A	0.385	0.018	/	3.01
Pu-239	0.105	0.148	0.108	0.070	N/A	0.044	0.323	/	0.38
SUM	2.87	2.99	0.18	0.06	N/A	0.39	0.33	/	3.0

b (pcm):

^{235}U : ~650

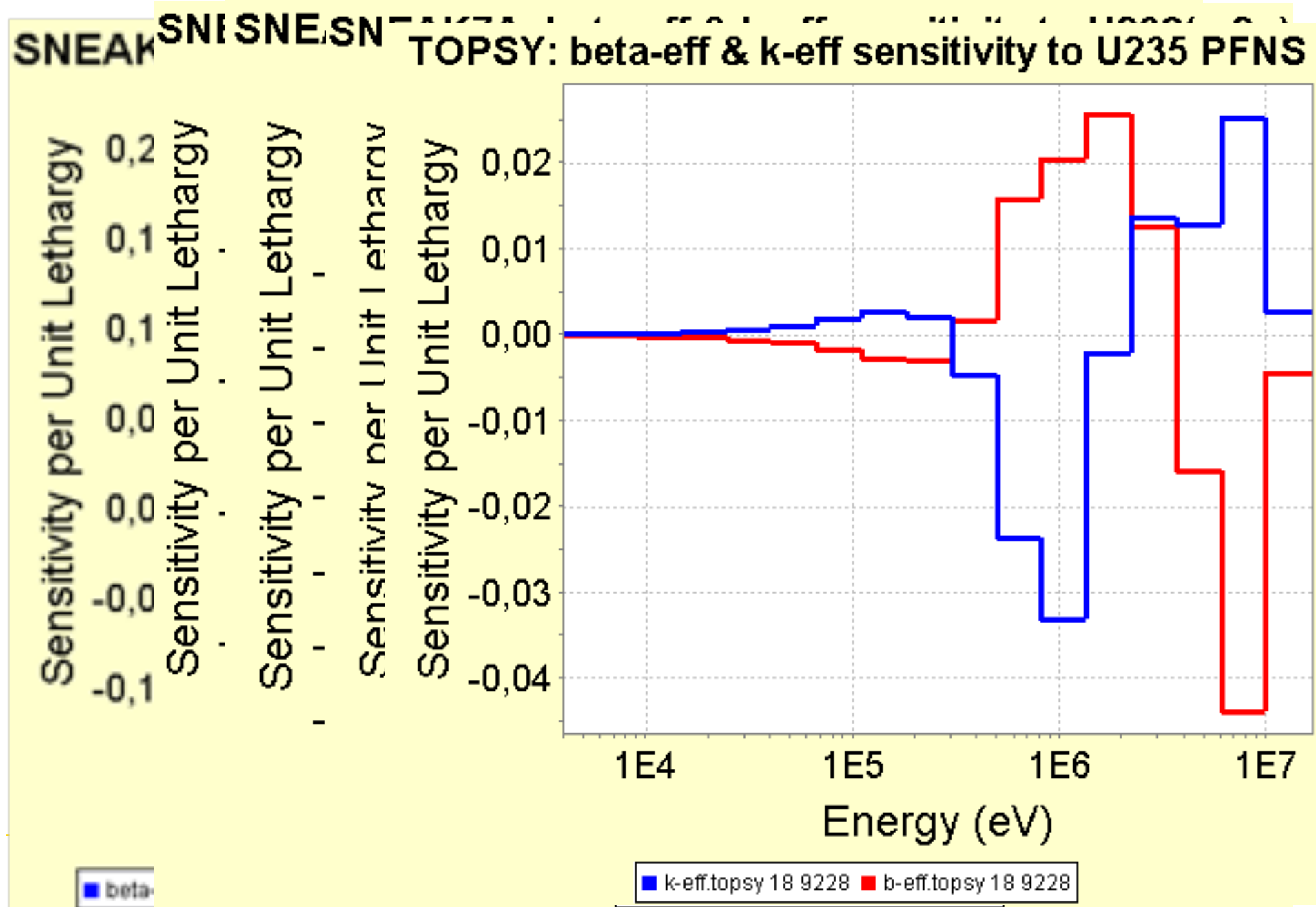
$^{238}\text{U}_f$: ~1480

^{239}Pu : ~210

^{240}Pu : ~270

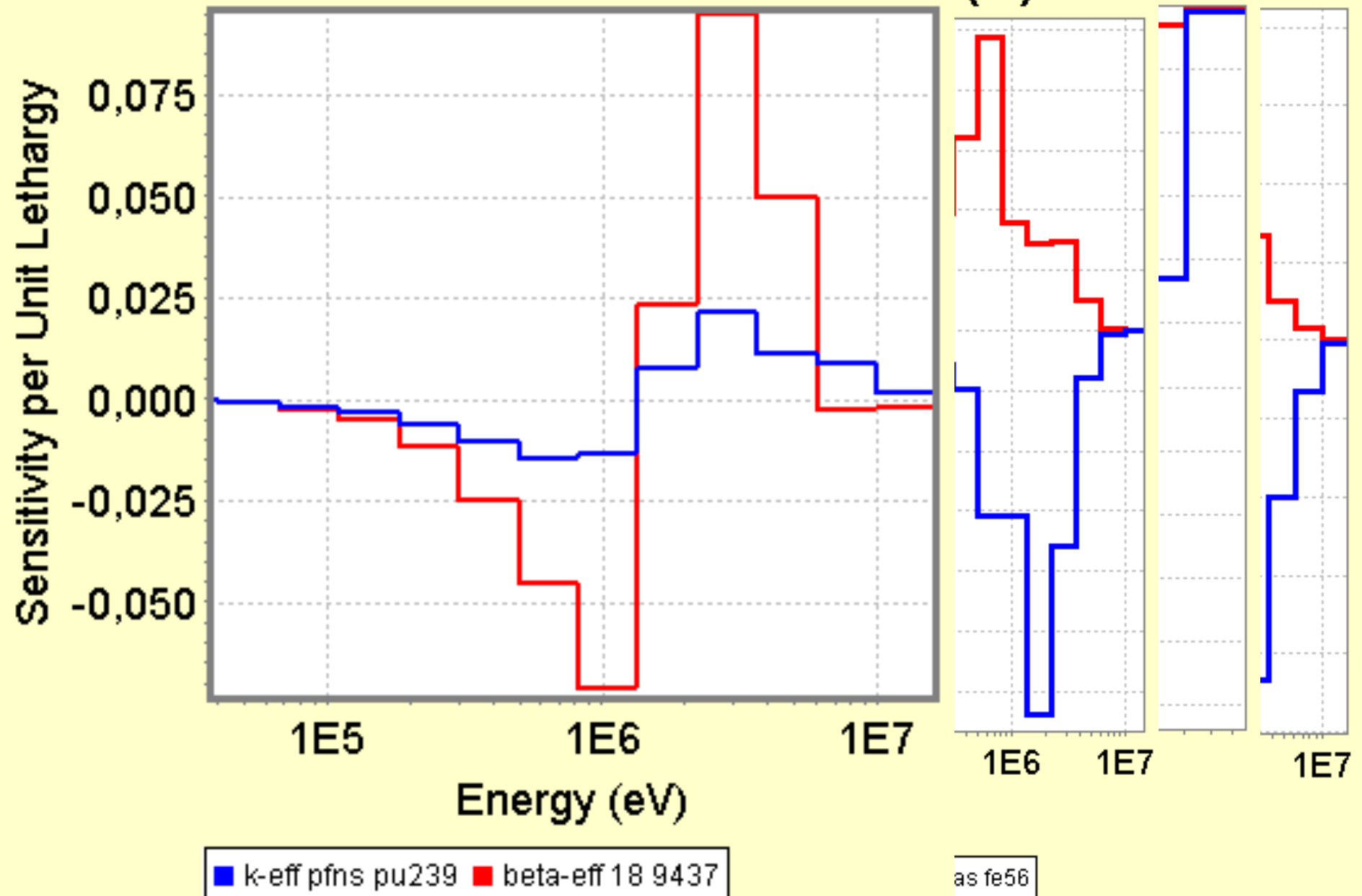
^{241}Pu : ~490

Differences in sensitivity profiles of b_{eff} and k_{eff}

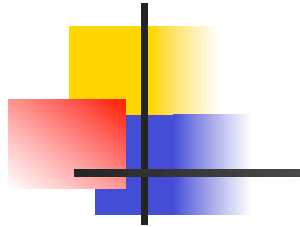


MYRRHA b_{eff} sensitivity / CHANDA

MYRRHA: k-eff & beta-eff sensitivity to pu239 PFNS $\phi(E)$

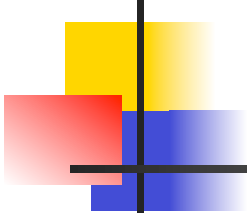


Calculated uncertainties k_{eff} vs. b_{eff} (%)



Assembly	Covariances	SUSD3D	
		k_{eff}	b_{eff} no/full corr.
SNEAK-7A	JENDL-4.0m	0.6144	2.7 / 3.8
	ENDF/B-VII.1	0.7671	
	SCALE6.0m	1.0897	
FLATTOP-Pu	JENDL-4.0m	0.7013	2.6 / 3.3
	ENDF/B-VII.1	0.5483	
	SCALE6.0m	1.2003	
JEZEBEL	JENDL-4.0m	0.6034	2.5 / 2.7
	ENDF/B-VII.1	0.5646	
	SCALE6.0m	1.3477	

Conclusions

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- **Use of shielding, criticality & kinetics benchmarks offers a more complete picture needed for ND validation.**
 - Powerful codes for nuclear data **sensitivity and uncertainty analysis**, both based on deterministic and Monte Carlo methods are available which, **combined with benchmark experiments, offer an efficient tool for evaluation and testing of nuclear data.**
 - The application of sensitivity and uncertainty tools to the effective delayed neutron fraction demonstrated the potential benefits of integrating the kinetics benchmarks into the nuclear data evaluation and validation schemes.
 - **Sensitivities of k_{eff} and b_{eff} show complementary features, suggesting that a combined use of both measurements can be optimal for the validation and improvement of modern nuclear data.**





CONCLUSIONS

- According to **JENDL-4.0m covariances**, the β_{eff} uncertainty is predominantly due to n_d uncertainties. In some cases (Popsy, SNEAK-7A, -7B, ZPPR-9, MYRRHA) the **inelastic & elastic scattering, (n,f) , n_p , ^{238}U and ^{235}U** play an important role.
- Uncertainty due to ^{238}U inelastic XS are almost twice as large using COMMARA-2 covariances (1.5–1.7% vs. 2.5–3%).
- **Total uncertainty in β_{eff} is $\sim 3\%$** (up to 5 - 7% for Flatop 23 due to ^{233}U uncertainties).
- Due to their high sensitivity and different shapes of sensitivity profiles the β_{eff} experiments can provide a complementary information to critical experiments for validation of e.g. on ^{238}U inelastic, elastic, fission, PFNS, in addition to n_d .
- **Challenges:**
 - **β_{eff} experimental uncertainty: 1 – 5% ??????**
 - **Improved covariance matrices needed: n_d + correlations among isotopes, DFNS**

